

In this worksheet, we study the motions of a fluid in a tank which is moved horizontally. These motions are described by the linearized Saint-Venant equations. See F. Dubois, N. Petit, P. Rouchon, *Motion planning and nonlinear simulations for a tank containing a fluid*, Proceedings of the European Control Conference, Karlsruhe, 1999 and N. Petit, P. Rouchon, *Motion Dynamics and Solutions to Some Control Problems for Water-Tank Systems*, IEEE Trans. Autom. Contr., vol. 47, no. 4, 2002, pp. 594-609.

```
> with(Ore_algebra):
> with(OreModules):
```

In order to write down the system matrix of the Saint-Venant equations, we define the Ore algebra Alg which contains the differential operator D w.r.t. time t and the operator δ which acts as a shift on the variable t . Without loss of generality, the length of the shift is taken to be 1.

```
> Alg := DefineOreAlgebra(diff=[D,t], dual_shift=[delta,s], polynom=[t,s],
> shift_action=[delta,t]):
```

We enter the system matrix of the Saint-Venant equations (which are shifted by 1 here):

```
> R := evalm([[delta^2, 1, -2*D*delta],[1, delta^2, -2*D*delta]]);
```

$$R := \begin{bmatrix} \delta^2 & 1 & -2D\delta \\ 1 & \delta^2 & -2D\delta \end{bmatrix}$$

The corresponding linear differential time-delay system is:

```
> ApplyMatrix(R, [phi1(t),phi2(t),phi3(t)], Alg)=evalm([[0],[0]]);
```

$$\begin{bmatrix} \phi_1(t-2) + \phi_2(t) - 2D(\phi_3)(t-1) \\ \phi_1(t) + \phi_2(t-2) - 2D(\phi_3)(t-1) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

We denote the Alg -module which is associated with this linear system by M . In order to check controllability and parametrizability of the system, we compute the first extension module with values in Alg of the transposed module of M (note that, since the system is time-invariant, we actually deal with matrices over a commutative polynomial ring, so we choose transposition of matrices as a trivial involution here).

```
> Ext1 := Exti(Involution(R, Alg), Alg, 1);
```

$$Ext1 := \left[\begin{bmatrix} \delta^2 - 1 & 0 \\ 0 & \delta^2 - 1 \end{bmatrix}, \begin{bmatrix} 1 & -1 & 0 \\ 0 & -\delta^2 - 1 & 2D\delta \end{bmatrix}, \begin{bmatrix} 2D\delta \\ 2D\delta \\ 1 + \delta^2 \end{bmatrix} \right]$$

Since $Ext1[1]$ is not an identity matrix, we find a generating set of torsion elements of M in $Ext1[2]$. Both rows r_1 and r_2 of $Ext1[2]$ are annihilated in M by $\delta^2 - 1$, i.e. $(\delta^2 - 1)r_i$ is zero modulo the rows of R , $i = 1, 2$. Hence, the torsion submodule $t(M)$ of M is non-trivial which means that the linear system described by the Saint-Venant equations is not controllable and not parametrizable. $Ext1[3]$ gives a parametrization of the torsion-free part $M / t(M)$ of M . The generating set of torsion elements can also be obtained by *TorsionElements* which expresses the torsion elements in terms of the system variables ϕ_1, ϕ_2, ϕ_3 :

```
> TorsionElements(R, [phi1(t),phi2(t),phi3(t)], Alg);
```

$$\left[\begin{bmatrix} \theta_1(t-2) - \theta_1(t) = 0 \\ \theta_2(t-2) - \theta_2(t) = 0 \end{bmatrix}, \begin{bmatrix} \theta_1(t) = \phi_1(t) - \phi_2(t) \\ \theta_2(t) = -\phi_2(t-2) - \phi_2(t) + 2D(\phi_3)(t-1) \end{bmatrix} \right]$$

Since M is not torsion-free, it is not projective and not free either. In what follows, we investigate whether the torsion submodule $t(M)$ has a complement in M , i.e. whether there exists a submodule C of M such that M is the direct sum of $t(M)$ and C . In the affirmative case, the complement C allows to construct a parametrization of M , although M corresponds to a linear system which has autonomous elements. A sufficient condition for this direct sum decomposition of M is that the torsion-free Alg -module $M / t(M)$ is projective. Let us check whether this simplest of all cases applies here:

```
> RightInverse(Ext1[2], Alg);
```

□

The matrix $Ext1[2]$ which presents the torsion-free part of M has full row rank, but does not admit a right-inverse. Hence, $M / t(M)$ is not projective. Note that the existence of a complement of $t(M)$ in M is equivalent to the fact that the short exact sequence $0 \rightarrow t(M) \rightarrow M \rightarrow M/t(M) \rightarrow 0$ splits, i.e., there exists an Alg -morphism $M/t(M) \rightarrow M$ which, composed by the canonical projection $M \rightarrow M/t(M)$, gives the identity on $M / t(M)$. The image of this morphism in M provides a complement of $t(M)$ in M . Let us check whether such a morphism exists:

```
> C := ComplementConstCoeff(Ext1[2], R, Alg);
```

$$C := \left[\begin{array}{ccc|cc} \frac{1}{2} & \frac{1}{2} & 0 & & \\ \frac{1}{2} & \frac{1}{2} & 0 & & \\ 0 & 0 & 1 & & \end{array} \right], \left[\begin{array}{cc} 0 & 0 \\ -\frac{1}{2} & -\frac{1}{2} \end{array} \right], \left[\begin{array}{cc} \frac{1}{2} & 0 \\ -\frac{1}{2} & 0 \\ 0 & 0 \end{array} \right]$$

We find one complement of $t(M)$ in M . It is generated by the residue classes of the rows of $C[1]$ in M .

```
> S := C[3]: V := C[2]:
```

In fact, the system of equations over Alg which *ComplementConstCoeff* has solved is $R' - R' S R' = V R$, where $R' = Ext1[2]$ and R were given and S and V were to be found. For more details see A. Quadrat, D. Robertz, *Parametrizing all solutions of controllable multidimensional linear systems*, Proceedings of the 16th IFAC World Congress, Prague, 2005.

```
> evalm(Ext1[2] - Mult(Ext1[2], S, Ext1[2], Alg) - Mult(V, R, Alg));
```

$$\begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

In order to construct a parametrization of M , we use the data just computed to glue the parametrization of the torsion-free part $M / t(M)$ with the “integration of the torsion elements” which follows first. We need to find the Alg -linear relations satisfied by the generating set of torsion elements $Ext1[2]$ in M (i.e., modulo the rows of R):

```
> SyzygyModule(linalg[stackmatrix](Ext1[2], R), Alg);
```

$$\begin{bmatrix} 1 & -1 & 0 & -1 \\ 0 & \delta^2 - 1 & -1 & \delta^2 \end{bmatrix}$$

The rows of the preceding result generate all linear relations that hold for the union of the rows of $Ext1[2]$ and R . So for each linear relation, the i th column gives the coefficient of the i th row of $Ext1[2]$, if $1 \leq i \leq 2$ and the $(2 + i)$ th column gives the coefficient of the i th row of R , $i = 1, 2$. Hence, we see from the first row of the preceding result, that the two torsion elements given by the rows of $Ext1[2]$ are equal modulo the rows of R . Hence, we have to solve $\theta_1(t - 2) - \theta_1(t) = 0$, $\theta_2 = \theta_1$. We find that θ_1 is any 2-periodic function of t and $\theta_2 = \theta_1$. A parametrization of M is then given by (see A. Quadrat, D.

Robertz, *Parametrizing all solutions of controllable multidimensional linear systems*, Proceedings of the 16th IFAC World Congress, Prague, 2005): $(\phi_1(t), \phi_2(t), \phi_3(t))^T = S(\theta_1(t), \theta_2(t))^T + Ext1[3]\xi_1$.

```
> P := evalm(ApplyMatrix(S, [theta[1](t), theta[2](t)], Alg) +
> ApplyMatrix(Ext1[3], [xi[1](t)], Alg));
```

$$P := \begin{bmatrix} \frac{1}{2}\theta_1(t) + 2D(\xi_1)(t-1) \\ -\frac{1}{2}\theta_1(t) + 2D(\xi_1)(t-1) \\ \xi_1(t) + \xi_1(t-2) \end{bmatrix}$$

We check that P is a parametrization of the system:

```
> ApplyMatrix(R, P, Alg);
```

$$\begin{bmatrix} \frac{1}{2}\theta_1(t-2) - \frac{1}{2}\theta_1(t) \\ \frac{1}{2}\theta_1(t) - \frac{1}{2}\theta_1(t-2) \end{bmatrix}$$

Since θ_1 is an arbitrary function of t which is 2-periodic, we see that the previous result is the zero vector, which proves that P is a parametrization of the Saint-Venant equations.

Now, we consider the linear system of the Saint-Venant equations over the Ore algebra $Alg2$ which contains the differential operator D w.r.t. time t , the shift operator δ and the operator τ which acts as an advance on the variable t :

```
> Alg2 := DefineOreAlgebra(diff=[D,t], 'shift+dual_shift'=[tau,delta,s],
> shift_action=[delta,t], shift_action=[tau,t], polynom=[s,t]);
```

The system matrix is then entered as follows:

```
> R2 := evalm([[delta, tau, -2*D], [tau, delta, -2*D]]);
```

$$R2 := \begin{bmatrix} \delta & \tau & -2D \\ \tau & \delta & -2D \end{bmatrix}$$

The corresponding linear differential time-delay system is:

```
> ApplyMatrix(R2, [phi1(t), phi2(t), phi3(t)], Alg2)=evalm([[0],[0]]);
```

$$\begin{bmatrix} \phi_1(t-1) + \phi_2(t+1) - 2D(\phi_3)(t) \\ \phi_1(t+1) + \phi_2(t-1) - 2D(\phi_3)(t) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

We denote the Alg 2-module which is associated with this linear system by $M2$. In order to compute the torsion submodule of $M2$, we compute the first extension module with values in $Alg2$ of the transposed module of $M2$ (note that we deal again with matrices over a commutative polynomial ring):

```
> Ext2 := Exti(Involution(R2, Alg2), Alg2, 1);
```

$$Ext2 := \left[\begin{bmatrix} \tau - \delta & 0 \\ 0 & \tau - \delta \end{bmatrix}, \begin{bmatrix} 1 & -1 & 0 \\ 0 & -\tau - \delta & 2D \end{bmatrix}, \begin{bmatrix} 2D \\ 2D \\ \tau + \delta \end{bmatrix} \right]$$

Hence, we find a generating set of torsion elements of $M2$ in $Ext2[2]$. When we compare $Ext2[2]$ and $Ext1[2]$, we see that the generators of $t(M2)$ are obtained from the generators of $t(M2)$ by shifting by 1. Of course, we obtain the rows of R by shifting the rows of $R2$ by 1 which explains the relationship. The generating torsion elements are expressed in terms of the system variables ϕ_1, ϕ_2, ϕ_3 now as follows:

```
> TorsionElements(R2, [phi1(t), phi2(t), phi3(t)], Alg2);
```

$$\left[\begin{array}{l} \theta_1(t+1) - \theta_1(t-1) = 0 \\ \theta_2(t+1) - \theta_2(t-1) = 0 \end{array} \right], \left[\begin{array}{l} \theta_1(t) = \phi_1(t) - \phi_2(t) \\ \theta_2(t) = -\phi_2(t+1) - \phi_2(t-1) + 2D(\phi_3)(t) \end{array} \right]$$

We investigate again whether or not $t(M2)$ has a complement in $M2$. First of all, we check whether $M2/t(M2)$ is projective:

```
> RightInverse(Ext2[2], Alg2);
```

□

Since $Ext2[2]$ has full row rank and does not admit a right-inverse, the torsion-free $Alg2$ -module $M2/t(M2)$ is not projective. Let us try to find S and V which satisfy $R' - R' S R' = V R2$, where $R' = Ext2[2]$:

```
> C := ComplementConstCoeff(Ext2[2], R2, Alg2);
```

$$C := \left[\begin{array}{ccc} \frac{1}{2} & \frac{1}{2} & 0 \\ \frac{1}{2} & \frac{1}{2} & 0 \\ 0 & 0 & 1 \end{array} \right], \left[\begin{array}{cc} 0 & 0 \\ -\frac{1}{2} & -\frac{1}{2} \end{array} \right], \left[\begin{array}{cc} \frac{1}{2} & 0 \\ -\frac{1}{2} & 0 \\ 0 & 0 \end{array} \right]$$

We find the same result as above.

```
> S := C[3]:
```

In order to construct a parametrization of $M2$, we compute the linear relations satisfied by the torsion elements given by $Ext2[2]$:

```
> SyzygyModule(linalg[stackmatrix](Ext2[2], R2), Alg2);
```

$$\left[\begin{array}{cccc} \delta & -1 & -1 & 0 \\ \tau & -1 & 0 & -1 \\ 0 & \tau - \delta & \tau & -\delta \end{array} \right]$$

Let us denote the torsion element given by the i th row of $Ext2[2]$ by θ_i , $i = 1, 2$. We find that θ_2 equals θ_1 advanced by 1. Hence, we have to solve (see the output of *TorsionElements*): $\theta_1(t+1) - \theta_1(t-1) = 0$, $\theta_2(t) = \theta_1(t-1)$. We find that θ_1 is any 2-periodic function of t and θ_2 equals θ_1 advanced by 1. Therefore, a parametrization of $M2$ is given by (see A. Quadrat, D. Robertz, *Parametrizing all solutions of controllable multidimensional linear systems*, Proceedings of the 16th IFAC World Congress, Prague, 2005): $(\phi_1(t), \phi_2(t), \phi_3(t))^T = S(\theta_1(t), \theta_2(t))^T + Ext2[3] \xi_1$.

```
> P2 := evalm(ApplyMatrix(S, [theta[1](t), theta[2](t)], Alg2) +
> ApplyMatrix(Ext2[3], [xi[1](t)], Alg2));
```

$$P2 := \left[\begin{array}{l} \frac{1}{2} \theta_1(t) + 2D(\xi_1)(t) \\ -\frac{1}{2} \theta_1(t) + 2D(\xi_1)(t) \\ \xi_1(t+1) + \xi_1(t-1) \end{array} \right]$$

Let us check that P is a parametrization of the system:

```
> ApplyMatrix(R2, P2, Alg2);
```

$$\begin{bmatrix} \frac{1}{2} \theta_1(t-1) - \frac{1}{2} \theta_1(t+1) \\ \frac{1}{2} \theta_1(t+1) - \frac{1}{2} \theta_1(t-1) \end{bmatrix}$$

Since θ_1 is a 2-periodic function of t , we see that P is a parametrization of the linearized Saint-Venant equations.

If we define $\pi = \theta_1/2$ and $v = 2\xi_1$, then the previous parametrization P of the system becomes the one obtained in (9) and (10) in F. Dubois, N. Petit, P. Rouchon, *Motion planning and nonlinear simulations for a tank containing a fluid*, Proceedings of the European Control Conference, Karlsruhe, 1999.

In N. Petit, P. Rouchon, *Motion Dynamics and Solutions to Some Control Problems for Water-Tank Systems*, IEEE Trans. Autom. Contr., vol. 47, no. 4, 2002, pp. 594-609, another model of a 1-D tank with a straight bottom and moving in translation is considered.

```
> Alg3 := DefineOreAlgebra(diff=[D,t], 'shift+dual_shift'=[tau,delta,s],
> shift_action=[delta,t], shift_action=[tau,t], polynom=[s,t], comm=[c,g]):
```

The system is defined by the following system matrix:

```
> R3 := evalm([[D*tau, -D*delta, (c/g)*D^2], [D*delta, -D*tau, (c/g)*D^2]]);
```

$$R3 := \begin{bmatrix} D\tau & -D\delta & \frac{cD^2}{g} \\ D\delta & -D\tau & \frac{cD^2}{g} \end{bmatrix}$$

The corresponding linear differential time-delay system is:

```
> ApplyMatrix(R3, [phi1(t), phi2(t), phi3(t)], Alg3)=evalm([[0],[0]]);
```

$$\begin{bmatrix} \frac{D(\phi_1)(t+1)g - D(\phi_2)(t-1)g + c(D^{(2)})(\phi_3)(t)}{g} \\ \frac{D(\phi_1)(t-1)g - D(\phi_2)(t+1)g + c(D^{(2)})(\phi_3)(t)}{g} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

We denote the $Alg3$ -module which is associated with this linear system by $M3$. In order to compute the torsion submodule of $M3$, we compute the first extension module with values in $Alg3$ of the transposed module of $M3$ (note that we deal again with matrices over a commutative polynomial ring):

```
> Ext3 := Exti(Involution(R3, Alg3), Alg3, 1);
```

$$Ext3 := \left[\begin{bmatrix} D\tau - D\delta & 0 \\ 0 & D\tau - D\delta \end{bmatrix}, \begin{bmatrix} 1 & 1 & 0 \\ 0 & -\tau g - \delta g & cD \end{bmatrix}, \begin{bmatrix} cD \\ -cD \\ -\tau g - \delta g \end{bmatrix} \right]$$

Hence, we find that $M3$ is not a torsion-free $Alg3$ -module. The generating torsion elements are expressed in terms of the system variables ϕ_1, ϕ_2, ϕ_3 as follows:

```
> TorsionElements(R3, [phi1(t), phi2(t), phi3(t)], Alg3);
```

$$\left[\begin{bmatrix} D(\theta_1)(t+1) - D(\theta_1)(t-1) = 0 \\ D(\theta_2)(t+1) - D(\theta_2)(t-1) = 0 \end{bmatrix}, \begin{bmatrix} \theta_1(t) = \phi_1(t) + \phi_2(t) \\ \theta_2(t) = -g\phi_2(t+1) - g\phi_2(t-1) + cD(\phi_3)(t) \end{bmatrix} \right]$$

Let us investigate again whether or not $t(M3)$ has a complement in $M3$. First of all, we check whether $M3 / t(M3)$ is projective:

> RightInverse(Ext3[2], Alg3);

□

Since $Ext3[2]$ has full row rank and does not admit a right-inverse, the torsion-free $Alg3$ -module $M3/t(M3)$ is not projective. Let us try to find S and V which satisfy $R' - R' S R' = V R3$, where $R' = Ext3[2]$:

> C3 := ComplementConstCoeff(Ext3[2], R3, Alg3);

C3 := []

We obtain that $t(M3)$ has no complement in $M3$. Therefore, we cannot glue the autonomous elements θ_1 and θ_2 of the system to the parametrization $Ext3[3]$ of the torsion-free $Alg3$ -module $M3 / t(M3)$ only by means of differential, delay and advance operators in order to parametrize the solutions of the system $R3(\eta_1, \eta_2, \eta_3)^T = 0$. Hence, a direct consequence of the lack of a splitting of $M3$ into a direct sum of $t(M3)$ and $M3 / t(M3)$ is that we cannot easily compute a parametrization of the system. Let us try to explain the obstruction.

We first factorize $R3$ by $Ext3[2]$:

> F := Factorize(R3, Ext3[2], Alg3);

$$F := \begin{bmatrix} D \tau & \frac{D}{g} \\ D \delta & \frac{D}{g} \end{bmatrix}$$

Therefore, we have $R3 = F Ext3[2]$, and thus, $R3 \eta = 0$ is equivalent to the inhomogeneous system $Ext3[2] \eta = \theta$ & $F \theta = 0$. Hence, we need to solve the following system:

> ApplyMatrix(F, [theta[1](t), theta[2](t)], Alg3)=evalm([[0], [0]]);

$$\begin{bmatrix} \frac{D(\theta_1)(t+1)g + D(\theta_2)(t)}{g} \\ \frac{D(\theta_1)(t-1)g + D(\theta_2)(t)}{g} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

which, after one integration, leads to the system

> ApplyMatrix(evalm(1/D*F), [theta[1](t), theta[2](t)], Alg3)=evalm([[c[1]], [c[2]]]);

$$\begin{bmatrix} \frac{\theta_1(t+1)g + \theta_2(t)}{g} \\ \frac{\theta_1(t-1)g + \theta_2(t)}{g} \end{bmatrix} = \begin{bmatrix} c_1 \\ c_2 \end{bmatrix}$$

where c_1 and c_2 are two arbitrary real constants. Subtracting the two equations, we can eliminate θ_2 and obtain the following equation in θ_1 :

> ApplyMatrix(evalm(linalg[submatrix](1/D*F, 1..1, 1..2)-
> linalg[submatrix](1/D*F, 2..2, 1..2)), [theta[1](t), theta[2](t)],
> Alg3)[1,1]=c[1]-c[2];

$$\theta_1(t+1) - \theta_1(t-1) = c_1 - c_2$$

Therefore, we need to solve the previous equation. A general solution of the homogeneous part is a 2-periodic function π . Moreover, we easily check that a particular solution of the inhomogeneous system is given by $\alpha(t) = (c_1 - c_2) \frac{t}{2}$. Hence, a general solution of the previous equation is of the form $\theta_1(t) = \pi(t) + \alpha(t)$.

Then, from the previous system, we can obtain θ_2 explicitly in terms of θ_1 as we have:

```
> Sol := solve(ApplyMatrix(evalm(1/D*F), [theta[1](t), theta[2](t)],
> Alg3)[2,1]=c[2], theta[2](t)): theta[2](t)=Sol;
theta(t) = -theta_1(t-1)g + c_2g
```

We finally obtain that $\theta_2(t) = (c_2 - \pi(t-1) - \alpha(t-1))g$, namely

```
> theta[2](t) := collect(collect(simplify(subs(
> theta[1](t-1)=pi(t-1)+(c[1]-c[2])*(t-1)/2, Sol)), t), g);
theta(t) := ((-1/2 c_1 + 1/2 c_2)t - pi(t-1) + 1/2 c_1 + 1/2 c_2)g
```

and θ_1 :

```
> theta[1](t) := pi(t)+(c[1]-c[2])*t/2;
theta(t) := pi(t) + 1/2 (c_1 - c_2)t
```

We now need to solve the inhomogeneous system $Ext3[2]\eta = \theta$, where $\theta = (\theta_1, \theta_2)^T$.

```
> ApplyMatrix(Ext3[2], [eta[1](t), eta[2](t), eta[3](t)], Alg3)
> =evalm([[theta[1](t)], [theta[2](t)]]);
```

$$\begin{bmatrix} \eta_1(t) + \eta_2(t) \\ -g\eta_2(t+1) - g\eta_2(t-1) + cD(\eta_3)(t) \end{bmatrix} = \begin{bmatrix} \pi(t) + \frac{1}{2}(c_1 - c_2)t \\ ((-\frac{1}{2}c_1 + \frac{1}{2}c_2)t - \pi(t-1) + \frac{1}{2}c_1 + \frac{1}{2}c_2)g \end{bmatrix}$$

```
> Ext3[2]=evalm([[theta[1](t)], [theta[2](t)]]);
```

The general solution of this system is then the sum of a particular solution of the inhomogeneous system and the general solution of the homogeneous system $Ext3[2]\eta = 0$.

The general solution of the homogeneous system $Ext3[2]\eta = 0$ is given by the parametrization $Ext3[3]$ or equivalently by:

```
> P3 := ApplyMatrix(Ext3[3], [xi[1](t)], Alg3);
P3 := \begin{bmatrix} cD(\xi_1)(t) \\ -cD(\xi_1)(t) \\ -g\xi_1(t+1) - g\xi_1(t-1) \end{bmatrix}
```

The fact that no splitting of $M3$ into a direct sum of $t(M3)$ and $M3 / t(M3)$ exists implies that there is no general algebraic way to obtain a particular solution of $Ext3[2]\eta = \theta$ using only θ and differential, delay and advance operators. However, we can check that a particular solution ζ of the inhomogeneous system $Ext3[2]\zeta = \theta$ is defined by:

```
> evalm([[zeta[1](t)], [zeta[2](t)], [zeta[3](t)]])=evalm([[pi(t)/2
> +(c[1]-c[2])*t/4+(c[1]+c[2])/4], [pi(t)/2+(c[1]-c[2])*t/4-(c[1]+c[2])/4], [0]]);
\begin{bmatrix} \zeta_1(t) \\ \zeta_2(t) \\ \zeta_3(t) \end{bmatrix} = \begin{bmatrix} \frac{1}{2}\pi(t) + \frac{1}{4}(c_1 - c_2)t + \frac{1}{4}c_1 + \frac{1}{4}c_2 \\ \frac{1}{2}\pi(t) + \frac{1}{4}(c_1 - c_2)t - \frac{1}{4}c_1 - \frac{1}{4}c_2 \\ 0 \end{bmatrix}
```

Indeed, if we compute $Ext3[2]\zeta$, we then get

```

> map(collect,ApplyMatrix(Ext3[2],[pi(t)/2+(c[1]-c[2])*t/4+(c[1]+c[2])/4,
> pi(t)/2+(c[1]-c[2])*t/4-(c[1]+c[2])/4,0],Alg3),{g,t,pi}, distributed);

```

$$\begin{bmatrix} \pi(t) + \left(\frac{1}{2}c_1 - \frac{1}{2}c_2\right)t \\ \left(\frac{1}{2}c_1 + \frac{1}{2}c_2\right)g - \frac{1}{2}g\pi(t-1) - \frac{1}{2}g\pi(t+1) + \left(-\frac{1}{2}c_1 + \frac{1}{2}c_2\right)tg \end{bmatrix}$$

and using the fact that π is 2-periodic, we find θ . Hence, we finally have the following parametrization of all the smooth solutions of the system $R^3(\eta_1, \eta_2, \eta_3)^T = 0$

```

> evalm([[eta[1](t)],[eta[2](t)],[eta[3](t)]])=evalm(P3+evalm([[pi(t)/2
> +(c[1]-c[2])*t/4+(c[1]+c[2])/4],[pi(t)/2+(c[1]-c[2])*t/4-(c[1]+c[2])/4],[0]]));

```

$$\begin{bmatrix} \eta_1(t) \\ \eta_2(t) \\ \eta_3(t) \end{bmatrix} = \begin{bmatrix} cD(\xi_1)(t) + \frac{1}{2}\pi(t) + \frac{1}{4}(c_1 - c_2)t + \frac{1}{4}c_1 + \frac{1}{4}c_2 \\ -cD(\xi_1)(t) + \frac{1}{2}\pi(t) + \frac{1}{4}(c_1 - c_2)t - \frac{1}{4}c_1 - \frac{1}{4}c_2 \\ -g\xi_1(t+1) - g\xi_1(t-1) \end{bmatrix}$$

where ξ_1 is an arbitrary smooth function, π a 2-periodic function and c_1 and c_2 two constants. We find again the parametrization of $R^3(\eta_1, \eta_2, \eta_3)^T = 0$ obtained in the paper N. Petit, P. Rouchon, *Motion Dynamics and Solutions to Some Control Problems for Water-Tank Systems*, IEEE Trans. Autom. Contr., vol. 47, no. 4, 2002, pp. 594-609. See page 599 for more details.