

Here we investigate a RLC-circuit which is composed of two resistances, one coil, and one condenser. See J.-F. Pommaret, *Partial Differential Control Theory*, Kluwer, 2001, p. 576.

```
> with(Ore_algebra):
> with(OreModules):
```

We define the Weyl algebra $Alg = A_1$, where D is the differential operator w.r.t. time t . Note that we have to declare all constants that occur in the system matrix by using the option *comm* in the definition of the Ore Algebra Alg .

```
> Alg := DefineOreAlgebra(diff=[D,t], polynom=[t], comm=[R1, R2, C, L]):
```

We enter the system matrix R :

```
> R := evalm([[D+1/(R1*C), 0, -1/(R1*C)], [0, D+R2/L, -1/L]]);
```

$$R := \begin{bmatrix} D + \frac{1}{R1 C} & 0 & -\frac{1}{R1 C} \\ 0 & D + \frac{R2}{L} & -\frac{1}{L} \end{bmatrix}$$

The formal adjoint R_{adj} of R is computed using *Involution*:

```
> R_adj := Involution(R, Alg);
```

$$R_{adj} := \begin{bmatrix} -D + \frac{1}{R1 C} & 0 \\ 0 & -D + \frac{R2}{L} \\ -\frac{1}{R1 C} & -\frac{1}{L} \end{bmatrix}$$

To check controllability of the RLC-circuit, we compute the first extension module ext^1 with values in Alg of the Alg -module which is associated with R_{adj} :

```
> Ext := Exti(R_adj, Alg, 1);
```

$$\text{Ext} := \left[\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \begin{bmatrix} D R1 C + 1 & 0 & -1 \\ 0 & D L + R2 & -1 \end{bmatrix}, \begin{bmatrix} D L + R2 \\ D R1 C + 1 \\ D L + L D^2 C R1 + R2 C R1 D + R2 \end{bmatrix} \right]$$

Since $\text{Ext}[1]$ is the identity matrix, we see that the torsion submodule $t(M)$ of the Alg -module M which is associated with the system is trivial *in the generic case*, i.e., the RLC-circuit is *generically* controllable (and, equivalently, parametrizable). This means that we have controllability for "almost all" choices of values for the constants $R1$, $R2$, C , L but there may be some configurations of the constants in which the RLC-circuit is not controllable. We shall actually find the only relation that leads to an uncontrollable system if the constants satisfy this relation.

Moreover, $\text{Ext}[3]$ is a parametrization of the system, namely we have $(x1 : x2 : u)^T = \text{Ext}[3] \xi$. We check whether this parametrization admits a left-inverse. In the affirmative case, we obtain a *flat output* of the system:

```
> S := LeftInverse(Ext[3], Alg);
```

$$S := \begin{bmatrix} -\frac{R1 C}{L - R1 C R2} & \frac{L}{L - R1 C R2} & 0 \end{bmatrix}$$

Hence, whenever $R1 C R2 - L \neq 0$, we find a flat output $\xi = S (x1 : x2 : u)^T$ of the system satisfies $(x1 : x2 : u)^T = Ext[3]\xi$. Then, the RLC-circuit is generically a flat system.

Let us point out that knowing the result of *Exti* above, it was already clear that the system is generically flat, because *Alg* is a principal ideal domain and torsion-free modules over principal ideal domains are free (and free modules correspond to flat systems).

The parametrization given in *Ext[3]*, can be obtained directly by using *Parametrization*:

> `Parametrization(R, Alg);`

$$\begin{bmatrix} R2 \xi_1(t) + L \left(\frac{d}{dt} \xi_1(t)\right) \\ \xi_1(t) + R1 C \left(\frac{d}{dt} \xi_1(t)\right) \\ R2 \xi_1(t) + L \left(\frac{d}{dt} \xi_1(t)\right) + \left(\frac{d}{dt} \xi_1(t)\right) R1 C R2 + L C R1 \left(\frac{d^2}{dt^2} \xi_1(t)\right) \end{bmatrix}$$

In fact, one directly gets the last result by applying *Ext[3]* to the free function ξ_1 :

> `ApplyMatrix(Ext[3], [xi[1](t)], Alg);`

$$\begin{bmatrix} R2 \xi_1(t) + L \left(\frac{d}{dt} \xi_1(t)\right) \\ \xi_1(t) + R1 C \left(\frac{d}{dt} \xi_1(t)\right) \\ R2 \xi_1(t) + (L + R1 C R2) \left(\frac{d}{dt} \xi_1(t)\right) + L C R1 \left(\frac{d^2}{dt^2} \xi_1(t)\right) \end{bmatrix}$$

> `SyzygyModule(R, Alg);`

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Therefore, R has full row rank. So we know that M is projective if and only if R admits a right-inverse:

> `T := RightInverse(R, Alg);`

$$T := \begin{bmatrix} \frac{L C R1}{L - R1 C R2} & -\frac{L^2}{L - R1 C R2} \\ \frac{R1^2 C^2}{L - R1 C R2} & -\frac{L C R1}{L - R1 C R2} \\ \frac{D R1^2 C^2 L}{L - R1 C R2} + \frac{R1^2 C^2 R2}{L - R1 C R2} & -\frac{C R1 D L^2}{L - R1 C R2} - \frac{L^2}{L - R1 C R2} \end{bmatrix}$$

> `simplify(Mult(R, T, Alg));`

$$\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

This right-inverse is well defined if and only if $R1 C R2 - L \neq 0$. Hence, we recover the same condition on the constants as above. If $R1 C R2 - L \neq 0$, then M is projective. Since the system is time-invariant, M is actually defined over the commutative polynomial ring with indeterminated D and t . By the theorem of Quillen and Suslin, we conclude that M is a free module, hence we see again that the system is flat.

Let us compute the Brunovský canonical form of the system in the case where $R1 C R2 - L \neq 0$.

> `B := Brunovsky(R, Alg);`

$$B := \begin{bmatrix} -\frac{R1 C}{L - R1 C R2} & \frac{L}{L - R1 C R2} & 0 \\ \frac{1}{L - R1 C R2} & -\frac{R2}{L - R1 C R2} & 0 \\ -\frac{1}{(L - R1 C R2) C R1} & \frac{R2^2}{(L - R1 C R2) L} & \frac{1}{L C R1} \end{bmatrix}$$

In other words, we have the following transformation between the system variables x_1 , x_2 and u and the Brunovský variables $z[i]$ and v :

> `evalm([seq([z[i](t)],i=1..2)],[v(t)])=ApplyMatrix(B, [x1(t),x2(t),u(t)], Alg);`

$$\begin{bmatrix} z_1(t) \\ z_2(t) \\ v(t) \end{bmatrix} = \begin{bmatrix} -\frac{R1 C x_1(t)}{L - R1 C R2} + \frac{L x_2(t)}{L - R1 C R2} \\ \frac{x_1(t)}{L - R1 C R2} - \frac{R2 x_2(t)}{L - R1 C R2} \\ -\frac{x_1(t)}{(L - R1 C R2) C R1} + \frac{R2^2 x_2(t)}{(L - R1 C R2) L} + \frac{u(t)}{L C R1} \end{bmatrix}$$

Let us check that the new variables $z[i]$ and v satisfy a Brunovský canonical form:

> `F := Elimination(linalg[stackmatrix](B, R), [x1,x2,u],`
 > `[seq(z[i],i=1..2),v,0,0], Alg):`
 > `ApplyMatrix(F[1], [x1(t),x2(t),u(t)], Alg)=`
 > `ApplyMatrix(F[2], [seq(z[i](t),i=1..2),v(t)], Alg);`

$$\begin{bmatrix} 0 \\ 0 \\ u(t) \\ x_2(t) \\ x_1(t) \end{bmatrix} = \begin{bmatrix} -\left(\frac{d}{dt} z_2(t)\right) + v(t) \\ -\left(\frac{d}{dt} z_1(t)\right) + z_2(t) \\ R2 z_1(t) + (R1 C R2 + L) z_2(t) + L C R1 v(t) \\ z_1(t) + R1 C z_2(t) \\ R2 z_1(t) + L z_2(t) \end{bmatrix}$$

Now, we study the case where $R1 C R2 = L$.

> `R_mod := subs(L=R1*R2*C, evalm(R));`

$$R_mod := \begin{bmatrix} D + \frac{1}{R1 C} & 0 & -\frac{1}{R1 C} \\ 0 & D + \frac{1}{R1 C} & -\frac{1}{R1 C R2} \end{bmatrix}$$

> `Ext_mod := Exti(Involution(R_mod, Alg), Alg, 1);`

$$Ext_mod := \left[\begin{bmatrix} D R1 C + 1 & 0 \\ 0 & 1 \end{bmatrix}, \begin{bmatrix} 1 & -R2 & 0 \\ 0 & R2 R1 C D + R2 & -1 \end{bmatrix}, \begin{bmatrix} -R2 \\ -1 \\ -R2 R1 C D - R2 \end{bmatrix} \right]$$

Hence, if $R1 C R2 = L$, then the RLC-circuit is not controllable. The generating set of torsion elements (which correspond to autonomous elements of the system) can also be obtained using *TorsionElements*. The generating torsion elements are expressed in terms of the dependent variables x_1 , x_2 , u of the system:

> `TorsionElements(R_mod, [x1(t),x2(t),u(t)], Alg);`

$$\left[\left[\theta_1(t) + R1 C \left(\frac{d}{dt} \theta_1(t)\right) = 0 \right], \left[\theta_1(t) = x_1(t) - R2 x_2(t) \right] \right]$$

We know that the torsion elements and the first integrals of motion are in one-to-one correspondence. Hence, let us compute a first integral of motion of the system.

> `V := FirstIntegral(R_mod, [x1(t),x2(t),u(t)], Alg);`

$$V := -\frac{C1 e^{\left(\frac{t}{R1 C}\right)} (x_1(t) - R2 x_2(t))}{R2}$$

Let us check that the derivative of V with respect to t is 0.

> `Vdot := diff(V,t);`

$$Vdot := -\frac{-C1 e^{(\frac{t}{R1C})} (x1(t) - R2 x2(t))}{R1 C R2} - \frac{-C1 e^{(\frac{t}{R1C})} ((\frac{d}{dt} x1(t)) - R2 (\frac{d}{dt} x2(t)))}{R2}$$

The equations of the system are given by:

> `Sys_mod := ApplyMatrix(R_mod, [x1(t),x2(t),u(t)], Alg) = evalm([[0],[0]]);`

$$Sys_mod := \begin{bmatrix} \frac{x1(t)}{R1 C} + (\frac{d}{dt} x1(t)) - \frac{u(t)}{R1 C} \\ \frac{x2(t)}{R1 C} + (\frac{d}{dt} x2(t)) - \frac{u(t)}{R1 C R2} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

From these equations, let us extract the first derivatives of $x1$ and $x2$:

> `lhs1 := solve(lhs(Sys_mod)[1,1], diff(x1(t),t));`

$$lhs1 := -\frac{x1(t) - u(t)}{R1 C}$$

> `lhs2 := solve(lhs(Sys_mod)[2,1], diff(x2(t),t));`

$$lhs2 := -\frac{R2 x2(t) - u(t)}{R1 C R2}$$

> `simplify(subs({diff(x1(t),t)=lhs1, diff(x2(t),t)=lhs2}, Vdot));`

0

Therefore, if we take into account the equations of the systems, $Vdot$ becomes 0, i.e., V is a first integral of motion.

Finally, let us compute the parametrization of the system defined by the matrix R by means of an arbitrary function ξ_1 and constants:

> `P := Parametrization(R_mod, Alg);`

$$P := \begin{bmatrix} -C1 e^{(-\frac{t}{R1C})} - R2 \xi_1(t) \\ -\xi_1(t) \\ -R2 (\xi_1(t) + R1 C (\frac{d}{dt} \xi_1(t))) \end{bmatrix}$$

We can check that P parametrizes some solutions of the system defined by R :

> `simplify(ApplyMatrix(R_mod, P, Alg));`

$$\begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

In fact, we can prove that P parametrizes all the C^∞ solutions. For more details, we refer the reader to A. Quadrat, D. Robertz, "On Monge problem for uncontrollable linear systems", to appear.

In (Pommaret, 2001) more examples for electric circuits are presented which can be treated analogously by using *OreModules*.