

Let us study the example of a flexible one-link robot following M. Benosman, G. Le Vey, *Accurate trajectory tracking of flexible arm end-point*, 6th IFAC Symposium on Robot Control, Vienna (Austria), 2000, pp. 569-572.

```
> with(Ore_algebra):
> with(OreModules):
```

Define the Weyl algebra $Alg = A_1$, where Dt acts as differential operator w.r.t. the variable t :

```
> Alg := DefineOreAlgebra(diff=[D,t], polynom=[t],
> comm=[M11,M12,M13,M21,M22,M31,M33,K1,K2,L,alpha,beta]):
```

The system matrix is defined by:

```
> R := evalm([[M11*D^2,M12*D^2,M13*D^2,-1],[M21*D^2,M22*D^2+K1,0,0],
> [M31*D^2,0,M33*D^2+K2,0]]);
```

$$R := \begin{bmatrix} M11 D^2 & M12 D^2 & M13 D^2 & -1 \\ M21 D^2 & M22 D^2 + K1 & 0 & 0 \\ M31 D^2 & 0 & M33 D^2 + K2 & 0 \end{bmatrix}$$

The corresponding system of ordinary differential equations is then given by

```
> ApplyMatrix(R, [theta(t),q1(t),q2(t),u(t)], Alg)=evalm([[0]$3]);
```

$$\begin{bmatrix} M11 \left(\frac{d^2}{dt^2} \theta(t)\right) + M12 \left(\frac{d^2}{dt^2} q1(t)\right) + M13 \left(\frac{d^2}{dt^2} q2(t)\right) - u(t) \\ M21 \left(\frac{d^2}{dt^2} \theta(t)\right) + K1 q1(t) + M22 \left(\frac{d^2}{dt^2} q1(t)\right) \\ M31 \left(\frac{d^2}{dt^2} \theta(t)\right) + K2 q2(t) + M33 \left(\frac{d^2}{dt^2} q2(t)\right) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

where M denotes the inertia matrix of the arm, $K1$ and $K2$ are the equivalent spring constants, θ is the joint variable, $q = (q1, q2)^T$ is the vector of modal coordinates and u is the torque applied to the beam hub. Let us check whether or not the system is controllable, parametrizable and flat.

We first introduce the formal adjoint R_{adj} of R .

```
> R_adj := Involution(R, Alg);
```

$$R_{adj} := \begin{bmatrix} M11 D^2 & M21 D^2 & M31 D^2 \\ M12 D^2 & M22 D^2 + K1 & 0 \\ M13 D^2 & 0 & M33 D^2 + K2 \\ -1 & 0 & 0 \end{bmatrix}$$

The system is controllable if and only if the Alg -module M associated with R is torsion-free, i.e., if and only if the first extension module ext^1 with values in Alg of the Alg -module associated with R_{adj} is the zero module. Let us check this last point.

```
> st := time(): Ext := Exti(R_adj, Alg, 1); time()-st;
```

$$\begin{aligned}
Ext := & \left[\begin{array}{ccc} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{array} \right], \\
& [-M33 D^2 M21 M12 - D^2 M22 M31 M13 + M33 D^2 M22 M11, -M33 M12 K1, \\
& -M13 M22 K2, -M33 M22] \\
& [0, M12 M31 K1, -K2 M21 M12 + K2 M22 M11 - M33 D^2 M21 M12 \\
& + M33 D^2 M22 M11 - D^2 M22 M31 M13, M22 M31] \\
& [0, -D^2 M22 M31 M13 + M33 D^2 M22 M11 - K1 M31 M13 - M33 D^2 M21 M12 \\
& + M33 K1 M11, M13 M21 K2, M33 M21], \\
& [M33 K1 D^2 + M33 D^4 M22 + K2 D^2 M22 + K1 K2] \\
& [-M33 D^4 M21 - K2 D^2 M21] \\
& [-K1 M31 D^2 - D^4 M22 M31] \\
& [M33 D^6 M22 M11 + M33 D^4 K1 M11 - M33 D^6 M21 M12 + K2 K1 M11 D^2 \\
& - D^4 K1 M31 M13 - D^6 M22 M31 M13 + K2 D^4 M22 M11 - K2 D^4 M21 M12]
\end{aligned}$$

0.459

Therefore, as the first matrix $Ext[1]$ is the identity, we obtain that the system is generically controllable, and thus, generically parametrizable. A parametrization is then given by $Ext[3]$ and we have:

> `evalm([[theta(t)], [q1(t)], [q2(t)], [u(t)]] = ApplyMatrix(Ext[3], [xi(t)], Alg);`

$$\begin{aligned}
& \begin{bmatrix} \theta(t) \\ q1(t) \\ q2(t) \\ u(t) \end{bmatrix} = \\
& \left[\begin{array}{l} K1 K2 \xi(t) + (M33 K1 + M22 K2) \left(\frac{d^2}{dt^2} \xi(t)\right) + M33 M22 \left(\frac{d^4}{dt^4} \xi(t)\right) \\ -K2 M21 \left(\frac{d^2}{dt^2} \xi(t)\right) - M33 M21 \left(\frac{d^4}{dt^4} \xi(t)\right) \\ -K1 M31 \left(\frac{d^2}{dt^2} \xi(t)\right) - M22 M31 \left(\frac{d^4}{dt^4} \xi(t)\right) \\ K2 K1 M11 \left(\frac{d^2}{dt^2} \xi(t)\right) \\ + (-K1 M31 M13 + M33 K1 M11 + K2 M22 M11 - K2 M21 M12) \left(\frac{d^4}{dt^4} \xi(t)\right) \\ + (-M33 M21 M12 + M33 M22 M11 - M22 M31 M13) \left(\frac{d^6}{dt^6} \xi(t)\right) \end{array} \right]
\end{aligned}$$

The fact that the Alg -module M associated with R is generically torsion-free implies that M is also projective as Alg is a hereditary ring. Projectivity of M can be verified by checking whether or not a right-inverse of R exists.

> `T := simplify(RightInverse(R, Alg));`

```

T :=
[0, -frac(M22^2 (M33 D^2 + K2), M21 K1 (-M33 K1 + M22 K2)), frac(M33^2 (M22 D^2 + K1), M31 K2 (-M33 K1 + M22 K2))]
[0, frac(M22 K2 - M33 K1 + M33 D^2 M22, K1 (-M33 K1 + M22 K2)), -frac(M33^2 D^2 M21, M31 K2 (-M33 K1 + M22 K2))]
[0, frac(M22^2 D^2 M31, M21 K1 (-M33 K1 + M22 K2)), -frac(M33 D^2 M22 - M33 K1 + M22 K2, K2 (-M33 K1 + M22 K2))]
[-1, -D^2(-K2 M22 M21 M12 + K2 M22^2 M11 - M13 M22^2 M31 D^2
- M22 D^2 M21 M12 M33 + M11 M22^2 D^2 M33 + M21 K1 M12 M33)/(M21 K1
(-M33 K1 + M22 K2)), D^2(-M33^2 D^2 M21 M12 + M33^2 D^2 M22 M11
- M33 M22 M31 D^2 M13 + M33^2 K1 M11 - M33 K1 M31 M13
+ M22 M31 K2 M13)/(M31 K2 (-M33 K1 + M22 K2))]
> Mult(R, T, Alg);

```

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Moreover, the fact that the system is time-invariant implies that the *Alg*-module M associated with R is generically free. Let us compute a basis of M .

```

> S := simplify(LeftInverse(Ext[3], Alg));
S := [frac(1, K1 K2), frac(M22^2, M21 K1 (-M33 K1 + M22 K2)), -frac(M33^2, M31 K2 (-M33 K1 + M22 K2)), 0]

```

Therefore, if $M33 K1 \neq M22 K2$, then the *Alg*-module M is free and, equivalently, the corresponding system is flat. Then, a basis of the *Alg*-module M (a *flat output* of the system) is defined by

```

> xi(t)=ApplyMatrix(S, [theta(t), q1(t), q2(t), u(t)], Alg)[1,1];
xi(t) = frac(theta(t), K1 K2) + frac(M22^2 q1(t), M21 K1 (-M33 K1 + M22 K2)) - frac(M33^2 q2(t), M31 K2 (-M33 K1 + M22 K2))

```

where ξ satisfies $(\theta, q1, q2, u)^T = Ext[3] \xi$. Let us compute the Brunovský canonical form in the case where $M33 K1 \neq M22 K2$.

```

> B := Brunovsky(R, Alg);

```

$$\begin{aligned}
B := & \begin{bmatrix} 1 & M22^2 & M33^2 \\ K1 K2 & M21 K1 (-M33 K1 + M22 K2) & -M31 K2 (-M33 K1 + M22 K2) \end{bmatrix}, 0 \\
& \begin{bmatrix} D & D M22^2 & D M33^2 \\ K1 K2 & M21 K1 (-M33 K1 + M22 K2) & -M31 K2 (-M33 K1 + M22 K2) \end{bmatrix}, 0 \\
& \begin{bmatrix} M22 & M33 \\ M21 (-M33 K1 + M22 K2) & M31 (-M33 K1 + M22 K2) \end{bmatrix}, 0 \\
& \begin{bmatrix} D M22 & M33 D \\ M21 (-M33 K1 + M22 K2) & M31 (-M33 K1 + M22 K2) \end{bmatrix}, 0 \\
& \begin{bmatrix} K1 & K2 \\ M21 (-M33 K1 + M22 K2) & -M31 (-M33 K1 + M22 K2) \end{bmatrix}, 0 \\
& \begin{bmatrix} K1 D & K2 D \\ M21 (-M33 K1 + M22 K2) & -M31 (-M33 K1 + M22 K2) \end{bmatrix}, 0 \\
& \begin{bmatrix} 0, \frac{K1 (-M33 K1 M11 + K2 M21 M12 + K1 M31 M13)}{M21 \%1 (-M33 K1 + M22 K2)}, \\ \frac{K2 (-K2 M21 M12 + K2 M22 M11 - K1 M31 M13)}{M31 \%1 (-M33 K1 + M22 K2)}, \frac{1}{\%1} \end{bmatrix} \\
\%1 := & M11 M22 M33 - M13 M22 M31 - M12 M21 M33
\end{aligned}$$

Equivalently, we obtain the following transformation between the Brunovsky variables $x[i]$, $i = 1, \dots, 6$, v and the system variables θ , $q1$, $q2$ and u .

```

> evalm([seq([x[i](t)], i=1..6), [v(t)]])=ApplyMatrix(B,
> [theta(t), q1(t), q2(t), u(t)], Alg);

```

$$\begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \\ x_4(t) \\ x_5(t) \\ x_6(t) \\ v(t) \end{bmatrix} = \begin{bmatrix} \frac{\theta(t)}{K1 K2} + \frac{M22^2 q1(t)}{M21 K1 (-M33 K1 + M22 K2)} - \frac{M33^2 q2(t)}{M31 K2 (-M33 K1 + M22 K2)} \\ \frac{\frac{d}{dt} \theta(t)}{K1 K2} + \frac{M22^2 (\frac{d}{dt} q1(t))}{M21 K1 (-M33 K1 + M22 K2)} - \frac{M33^2 (\frac{d}{dt} q2(t))}{M31 K2 (-M33 K1 + M22 K2)} \\ \left[-\frac{M22 q1(t)}{M21 (-M33 K1 + M22 K2)} + \frac{M33 q2(t)}{M31 (-M33 K1 + M22 K2)} \right] \\ \left[-\frac{M22 (\frac{d}{dt} q1(t))}{M21 (-M33 K1 + M22 K2)} + \frac{M33 (\frac{d}{dt} q2(t))}{M31 (-M33 K1 + M22 K2)} \right] \\ \left[\frac{K1 q1(t)}{M21 (-M33 K1 + M22 K2)} - \frac{K2 q2(t)}{M31 (-M33 K1 + M22 K2)} \right] \\ \left[\frac{K1 (\frac{d}{dt} q1(t))}{M21 (-M33 K1 + M22 K2)} - \frac{K2 (\frac{d}{dt} q2(t))}{M31 (-M33 K1 + M22 K2)} \right] \\ \left[\frac{K1 (-M33 K1 M11 + K2 M21 M12 + K1 M31 M13) q1(t)}{M21 \%1 (-M33 K1 + M22 K2)} \right. \\ \left. + \frac{K2 (-K2 M21 M12 + K2 M22 M11 - K1 M31 M13) q2(t)}{M31 \%1 (-M33 K1 + M22 K2)} + \frac{u(t)}{\%1} \right] \\ \%1 := M11 M22 M33 - M13 M22 M31 - M12 M21 M33
\end{bmatrix}$$

We easily check that, in the Brunovský coordinates, the system becomes the following Brunovský canonical system.

```

> E := Elimination(linalg[stackmatrix](B, R), [theta,q1,q2,u],
> [seq(x[i],i=1..6),v,0,0,0], Alg):
> ApplyMatrix(E[1], [theta(t),q1(t),q2(t),u(t)], Alg)=ApplyMatrix(E[2],
> [seq(x[i](t),i=1..6), v(t)], Alg);

```

$$\begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ u(t) \\ q2(t) \\ q1(t) \\ \theta(t) \end{bmatrix} = \begin{bmatrix} -\left(\frac{d}{dt} x_6(t)\right) + v(t) \\ -\left(\frac{d}{dt} x_5(t)\right) + x_6(t) \\ -\left(\frac{d}{dt} x_4(t)\right) + x_5(t) \\ -\left(\frac{d}{dt} x_3(t)\right) + x_4(t) \\ -\left(\frac{d}{dt} x_2(t)\right) + x_3(t) \\ -\left(\frac{d}{dt} x_1(t)\right) + x_2(t) \\ \left[K2 K1 M11 x_3(t) \right. \\ \left. + (M33 K1 M11 - K2 M21 M12 - K1 M31 M13 + K2 M22 M11) x_5(t) \right. \\ \left. + (M11 M22 M33 - M13 M22 M31 - M12 M21 M33) v(t) \right] \\ -K1 M31 x_3(t) - M22 M31 x_5(t) \\ -M21 K2 x_3(t) - M33 M21 x_5(t) \\ \left. \left[K1 K2 x_1(t) + (M33 K1 + M22 K2) x_3(t) + M33 M22 x_5(t) \right] \right]
\end{bmatrix}$$

The output is chosen to be the linear position of the end-effector.

```

> Ry := evalm([[L,alpha,beta,0]]);
              Ry := [ L  alpha  beta  0 ]
> y(t)=ApplyMatrix(Ry, [theta(t),q1(t),q2(t),u(t)], Alg)[1,1];
              y(t) = L theta(t) + alpha q1(t) + beta q2(t)

```

Let us compute the input-output behaviour of the system.

```

> IO := Elimination(linalg[stackmatrix](R, Ry), [theta,q1,q2,u],
> [seq(0,i=1..3),y], Alg, [u]):
> ApplyMatrix(linalg[submatrix](IO[2], 1..1, 1..2), [y(t),u(t)],
> Alg)[1,1]=0;

```

$$\begin{aligned}
& -K2 K1 M11 \left(\frac{d^2}{dt^2} y(t)\right) \\
& + (-K2 M22 M11 + K2 M21 M12 - M33 K1 M11 + K1 M31 M13) \left(\frac{d^4}{dt^4} y(t)\right) \\
& + (-M11 M22 M33 + M13 M22 M31 + M12 M21 M33) \left(\frac{d^6}{dt^6} y(t)\right) + K2 K1 L u(t) \\
& + (L M33 K1 + L K2 M22 - K2 M21 \alpha - M31 K1 \beta) \left(\frac{d^2}{dt^2} u(t)\right) \\
& + (-M31 \beta M22 + L M33 M22 - M21 M33 \alpha) \left(\frac{d^4}{dt^4} u(t)\right) = 0
\end{aligned}$$

Let us quickly study the particular case where $M33 K1 = M22 K2$. The system matrix becomes:

```

> R_bis := subs(K2=(M33*K1)/M22, evalm(R));

```

$$R_{bis} := \begin{bmatrix} M11 D^2 & M12 D^2 & M13 D^2 & -1 \\ M21 D^2 & M22 D^2 + K1 & 0 & 0 \\ M31 D^2 & 0 & M33 D^2 + \frac{M33 K1}{M22} & 0 \end{bmatrix}$$

The formal adjoint R_{bisadj} of R_{bis} is defined by:

> $R_{bisadj} := \text{Involution}(R_{bis}, \text{Alg});$

$$R_{bisadj} := \begin{bmatrix} M11 D^2 & M21 D^2 & M31 D^2 \\ M12 D^2 & M22 D^2 + K1 & 0 \\ M13 D^2 & 0 & M33 D^2 + \frac{M33 K1}{M22} \\ -1 & 0 & 0 \end{bmatrix}$$

The previous study shows that the Alg -module M_{bis} associated with R_{bis} contains some torsion elements, and thus, the corresponding system has some autonomous elements. Let us check these results.

> $\text{TorsionElements}(R_{bis}, [\text{theta}(t), \text{q1}(t), \text{q2}(t), \text{u}(t)], \text{Alg});$

$$\left[\begin{array}{l} \left[\begin{array}{l} K1 \theta_1(t) + M22 \left(\frac{d^2}{dt^2} \theta_1(t) \right) = 0 \\ K1 \theta_2(t) + M22 \left(\frac{d^2}{dt^2} \theta_2(t) \right) = 0 \\ K1 \theta_3(t) + M22 \left(\frac{d^2}{dt^2} \theta_3(t) \right) = 0 \end{array} \right], \\ \theta_1(t) = \\ (M11 M22^2 M33 M31 - M13 M22^2 M31^2 - M31 M22 M12 M21 M33) \left(\frac{d^2}{dt^2} \theta(t) \right) \\ + (-M13 M22 M31 M33 K1 - M12 M21 M33^2 K1) \text{q2}(t) - M22^2 M33 M31 \text{u}(t) \\ \theta_2(t) = M22 M31 \text{q1}(t) - M33 M21 \text{q2}(t) \\ \theta_3(t) = M33 K1 M11 \text{q2}(t) \\ \\ + (M11 M22 M33 - M13 M22 M31 - M12 M21 M33) \left(\frac{d^2}{dt^2} \text{q2}(t) \right) + M22 M31 \text{u}(t) \end{array} \right]$$

> $\text{Auto} := \text{AutonomousElements}(R_{bis}, [\text{theta}(t), \text{q1}(t), \text{q2}(t), \text{u}(t)], \text{Alg});$

$$\begin{aligned}
\text{Auto} := & \left[\begin{array}{l} \theta_1(t) + M33 M22 \theta_3(t) = 0 \\ M12 K1 \theta_2(t) + M22 \theta_3(t) = 0 \\ K1 \theta_3(t) + M22 \left(\frac{d^2}{dt^2} \theta_3(t)\right) = 0 \end{array} \right], \left[\begin{array}{l} \theta_1 = -M33 M22 \%1 \\ \theta_2 = -\frac{M22 \%1}{M12 K1} \\ \theta_3 = \%1 \end{array} \right], \\
& \left[\begin{array}{l} \theta_1 = \\ (M11 M22^2 M33 M31 - M13 M22^2 M31^2 - M31 M22 M12 M21 M33) \left(\frac{d^2}{dt^2} \theta(t)\right) \\ + (-M13 M22 M31 M33 K1 - M12 M21 M33^2 K1) q2(t) - M22^2 M33 M31 u(t) \\ \theta_2 = M22 M31 q1(t) - M33 M21 q2(t) \\ \left[\theta_3 = M33 K1 M11 q2(t) \right. \\ \left. + (M11 M22 M33 - M13 M22 M31 - M12 M21 M33) \left(\frac{d^2}{dt^2} q2(t)\right) + M22 M31 u(t) \right] \end{array} \right] \\
\%1 := & _C1 \sin\left(\frac{\sqrt{K1} t}{\sqrt{M22}}\right) + _C2 \cos\left(\frac{\sqrt{K1} t}{\sqrt{M22}}\right)
\end{aligned}$$

The second matrix *Auto*[2] gives the autonomous elements. Moreover, the third matrix *Auto*[3] gives the expression of the autonomous elements in terms of the system variables θ , $q1$, $q2$ and u whereas the first one *Auto*[1] corresponds to the system that they satisfy.

Let us recall that the autonomous elements are in one-to-one correspondence with the first integrals of the system. Let us compute the generic first integral of the system.

> `FirstIntegral(R_bis, [theta(t),q1(t),q2(t),u(t)], Alg);`

$$\begin{aligned}
& -(M22^{(3/2)} M31 \left(\frac{d}{dt} q1(t)\right) _C1 \sin\left(\frac{\sqrt{K1} t}{\sqrt{M22}}\right) + M22^{(3/2)} M31 \left(\frac{d}{dt} q1(t)\right) _C2 \cos\left(\frac{\sqrt{K1} t}{\sqrt{M22}}\right) \\
& - M22 q1(t) M31 _C1 \cos\left(\frac{\sqrt{K1} t}{\sqrt{M22}}\right) \sqrt{K1} + M22 q1(t) M31 _C2 \sin\left(\frac{\sqrt{K1} t}{\sqrt{M22}}\right) \sqrt{K1} \\
& - M33 \left(\frac{d}{dt} q2(t)\right) _C1 \sin\left(\frac{\sqrt{K1} t}{\sqrt{M22}}\right) M21 \sqrt{M22} \\
& - M33 \left(\frac{d}{dt} q2(t)\right) _C2 \cos\left(\frac{\sqrt{K1} t}{\sqrt{M22}}\right) M21 \sqrt{M22} \\
& + M33 q2(t) _C1 \cos\left(\frac{\sqrt{K1} t}{\sqrt{M22}}\right) \sqrt{K1} M21 - M33 q2(t) _C2 \sin\left(\frac{\sqrt{K1} t}{\sqrt{M22}}\right) \sqrt{K1} M21 \\
& / (M21 \sqrt{M22})
\end{aligned}$$

We now consider the same system but with a constant time-delay in the input u due, for instance, to a teleoperation process. We first define the Ore algebra of differential time-delay operators.

> `Alg2 := DefineOreAlgebra(diff=[D,t], dual_shift=[delta,s], polynom=[t,s],`
> `comm=[M11,M12,M13,M21,M22,M31,M33,K1,K2], shift_action=[delta,t,h]);`

The matrix which defines the system is then given by:

> `R2 := evalm([[M11*D^2,M12*D^2,M13*D^2,-delta],[M21*D^2,M22*D^2+K1,0,0],`
> `[M31*D^2,0,M33*D^2+K2,0]]);`

$$R2 := \begin{bmatrix} M11 D^2 & M12 D^2 & M13 D^2 & -\delta \\ M21 D^2 & M22 D^2 + K1 & 0 & 0 \\ M31 D^2 & 0 & M33 D^2 + K2 & 0 \end{bmatrix}$$

We define the formal adjoint $R2_adj$ of $R2$ using an involution of $Alg2$.

> $R2_adj := \text{Involution}(R2, Alg2):$

Let us check whether or not the system is controllable, parametrizable and flat. In order to do that, let us check whether or not the $Alg2$ -module associated with $R2$ is torsion-free.

> $Ext1 := \text{Exti}(R2_adj, Alg2, 1);$

$$Ext1 := \left[\begin{array}{l} \left[\begin{array}{ccc} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{array} \right], \\ [-M33 D^2 M21 M12 - D^2 M22 M31 M13 + M33 D^2 M22 M11, -M33 M12 K1, \\ -M13 M22 K2, -M33 \delta M22] \\ [0, M12 M31 K1, -K2 M21 M12 + K2 M22 M11 - M33 D^2 M21 M12 \\ + M33 D^2 M22 M11 - D^2 M22 M31 M13, M22 M31 \delta] \\ [0, -D^2 M22 M31 M13 + M33 D^2 M22 M11 - K1 M31 M13 - M33 D^2 M21 M12 \\ + M33 K1 M11, M13 M21 K2, M33 M21 \delta], \\ [M33 D^4 \delta M22 + M33 K1 \delta D^2 + K1 \delta K2 + K2 \delta M22 D^2] \\ [-M33 M21 \delta D^4 - M21 D^2 \delta K2] \\ [-D^4 M22 M31 \delta - \delta M31 K1 D^2] \\ [M33 D^6 M22 M11 + M33 D^4 K1 M11 - M33 D^6 M21 M12 + K2 K1 M11 D^2 \\ - D^4 K1 M31 M13 - D^6 M22 M31 M13 + K2 D^4 M22 M11 - K2 D^4 M21 M12] \end{array} \right]$$

As the first matrix $Ext1[1]$ is the identity, we deduce that the system is generically controllable and parametrizable. A parametrization is then defined by:

> $\text{evalm}([\theta(t)], [q1(t)], [q2(t)], [u(t)]) = \text{ApplyMatrix}(Ext1[3], [xi(t)], Alg2);$

$$\begin{bmatrix} \theta(t) \\ q1(t) \\ q2(t) \\ u(t) \end{bmatrix} = \begin{array}{l} [M33 M22 (D^{(4)})(\xi)(t-h) + M33 K1 \%1 + K1 K2 \xi(t-h) + M22 K2 \%1] \\ [-M33 M21 (D^{(4)})(\xi)(t-h) - M21 K2 \%1] \\ [-M22 M31 (D^{(4)})(\xi)(t-h) - K1 M31 \%1] \\ [M11 M22 M33 (D^{(6)})(\xi)(t) + M33 K1 M11 (D^{(4)})(\xi)(t) \\ - M12 M21 M33 (D^{(6)})(\xi)(t) + K2 K1 M11 (D^{(2)})(\xi)(t) \\ - K1 M31 M13 (D^{(4)})(\xi)(t) - M13 M22 M31 (D^{(6)})(\xi)(t) \\ + K2 M22 M11 (D^{(4)})(\xi)(t) - K2 M21 M12 (D^{(4)})(\xi)(t)] \\ \%1 := (D^{(2)})(\xi)(t-h) \end{array}$$

Let us check whether or not the system is flat. In order to do that, we need to check whether or not the $Alg2$ -module associated with $R2$ is projective.

```
> Ext2 := Exti(R2_adj, Alg2, 2);
```

```
Ext2 := [
[delta]
[M33 D^6 M22 M11 + M33 D^4 K1 M11 - M33 D^6 M21 M12 + K2 K1 M11 D^2
- D^4 K1 M31 M13 - D^6 M22 M31 M13 + K2 D^4 M22 M11 - K2 D^4 M21 M12],
[ 1 ], SURJ(1)]
```

As the first matrix $Ext2[1]$ is different from the identity matrix, we obtain that the system is not flat. As the torsion-free degree of the $Alg2$ -module associated with $R2$ is 1, we know that there is a π -polynomial in δ . Let us compute it.

```
> PiPolynomial(R2, Alg2, [delta]);
```

```
[delta]
```

Therefore, if we allow the time-advance operator δ^{-1} in the system, then the system becomes flat. In particular, a flat output of the system is defined by computing a left-inverse of the parametrization $Ext1[3]$ of the system over $Alg2[\delta^{-1}]$. Let us compute such a left-inverse.

```
> S2 := LocalLeftInverse(Ext1[3], [delta], Alg2);
```

$$S2 := \begin{bmatrix} 1 & M22^2 & M33^2 & 0 \\ \delta K1 K2 & \delta M21 K1 (-M33 K1 + M22 K2) & -\delta M31 K2 (-M33 K1 + M22 K2) & 0 \end{bmatrix}$$

Then, the flat output of the system is defined by:

```
> psi(t)=ApplyMatrix(S2, [theta(t),q1(t),q2(t),u(t)], Alg2)[1,1];
```

$$\psi(t) = \frac{\theta(t+h)}{K1 K2} + \frac{M22^2 q1(t+h)}{M21 K1 (-M33 K1 + M22 K2)} - \frac{M33^2 q2(t+h)}{M31 K2 (-M33 K1 + M22 K2)}$$

Let us point out that this flat output corresponds exactly to the advanced flat output of the first model, i.e., without the time-delay in the input of the system.